

SEVERAL OPEN PROBLEMS IN PARALLEL ROBOTICS

ABSTRACT:

More than 20 years parallel robots attract the interest of the scientific community and in many applicative domains like, production of motion generators, machine tools, precision positioning devices, medical equipment, pick and place machines, etc., where their potential advantages (high accuracy, rigidity, speed, acceleration and load carrying capability) could be very useful. The objective of this paper is to notify some of the open questions in parallel robotics, which is limitation factor of wider practical application of this type of robots.

KEYWORDS:

parallel robots, open problems, research

INTRODUCTION

A parallel robot is composed of two or more closed-loop kinematic chains in which the end-effector (mobile platform) is connected to the base (fixed platform) by at least two independent kinematic chains. Between the base and end-effector platforms are serial chains (called limbs or legs) [90] (fig. 1). Parallel robot could be named as hexapod, a Stewart platform, Gough platform, Stewart-Gough platform, a parallel kinematic machine (PKM) or a parallel manipulator. Theoretical work on parallel mechanisms dates back to as early as 1645 by Christopher Wren, then in 1813 by Cauchy and in 1867 by Lebesgue. Variable-length-strut hexapods, as those used in motion simulators [31,84] have existed almost 50 years.

Parallel mechanisms are stronger than serial because the load is distributed among all legs, but also because, for some architectures, the legs are only subjected to axial loads. Also, parallel robots theoretically should be more precise since they are more rigid, and since the errors in the legs are averaged instead of accumulated. Finally, these robots are faster since they usually have their heavy motors mounted on the base (fig. 1)

On the other hand, parallel robots have a more limited and complex-shaped workspace. Moreover, the rotation and position capabilities (if both present) of parallel mechanisms are highly coupled which makes their control and calibration extremely complex. Furthermore, parallel mechanisms generally have singularities within their workspace and computing the resulting end-effector position for a given set of actuator inputs is, in general, a very difficult and complex problem allowing up to 40 solutions.

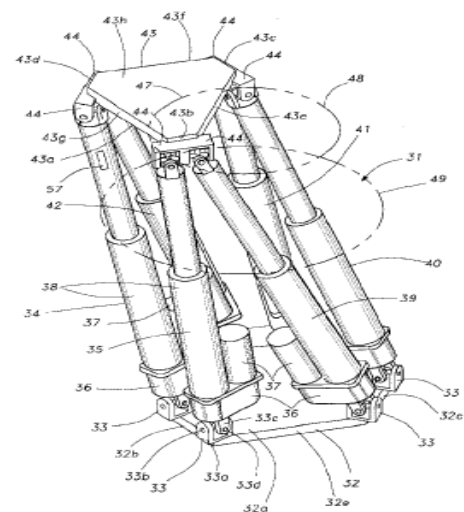


FIGURE 1. A FANUC parallel robot [94] (US patent No. 5987726) [93]

General overview of the main characteristics of the parallel robots are given in the table below:

Table 1.

Feature	Parallel robot
Workspace	Small and complex
Solving forward kinematics	Very difficult
Solving inverse kinematic	Easy
Position error	Averages
Force error	Accumulates
Maximum force	Summation of all actuator forces
Stiffness	High
Dynamics characteristics	Very high
Modelling and solving dynamics	Very complex
Inertia	Small
Areas of application	Currently limited, especially in industry
Payload/weight ratio	High
Speed and acceleration	High
Accuracy	High
Uniformity of components	High
Calibration	Complicated
Workspace/robot size ratio	Low

In the past two decades parallel robots very much attracted the interest in the robotics community. Great interest for parallel robots come from the potentially interesting features of parallel mechanisms: high accuracy, rigidity, speed and large load carrying capability, which in a very large number of cases may overcome the drawbacks of the more complex kinematics, dynamics and smaller workspace. The great interest could be exemplified by a large number of papers published on this subject together with the application of parallel robots in very different domains such as fine positioning devices, simulators, motion generators (platforms), ultra-fast pick and place robots, machine-tools, medical applications, haptic devices, entertainment, force sensors, micro-robots, etc.

But in fact all these advantages of parallel robots are only potential. Any real parallel robot will present in practice impressing performances only if all its components (either hardware or software) present a high level of performance. However in many cases unexpected difficulties in the design and control of such complex system have led to performances which, although still better than conventional serial mechanical architectures, were far below what was expected. In some cases, for example, the machine tools, performances were even the worst [89].

In the following we will give some examples of some open problems in parallel robotics, which makes limitation of wider practical application of this type of robots.

OPEN QUESTIONS IN PARALLEL ROBOTICS

Mechanical design

A lot of different mechanical architectures of parallel robots, more than 100 according [60] with 2 to 6 DOF have already been proposed and it is probable that not all of them have been discovered. Analysis of the

literature shows that more than 80% of the parallel robots are with 3 DOF and 6 DOF. The rest are parallel robots with 5 DOF, 4 DOF, and 2DOF. Unfortunately there are not so many proposed architecture that have only 4 or 5 DOF, while many applications require such number of DOF. For example 4-DOF is sufficient for most pick-and place applications, and 5-DOF is adequate for every machine tool application.

There is a recent trend is to propose parallel robots with 4 and 5 DOF: [19, 69, 16, 18, 26, 50, 99, 21, 98, 104, 10].

It is really an interesting research area but many questions arise with this type of robots:

- ❖ the proposed structures have in theory only 4 or 5 DOF and rely on geometrical constraints to obtain this reduced number of DOF. In practice however these constraints will never be perfectly fulfilled and hence these robots will exhibit parasitic motions. Open problems are to determine what will be the maximal amplitude of these parasitic motion, produced by given manufacturing tolerances, [11, 33] and the dual problem of determining the amplitude of the manufacturing tolerances so that the maximal amplitude of the parasitic motion will not exceed a given limits.

- ❖ having less actuators and sensors may sound economically interesting, but it is unclear, if classical parallel robots with 6 DOF which are redundant with respect to the task, are more appropriated. First of all their kinematic chains are identical (which is not the case for the most of 4 and 5 DOF robots). That will reduce the maintenance costs. Then by using the redundancy it is possible to optimize the performances of the robot for a given task

Redundancy is also an interesting and open research area. In the field of parallel robots redundancy has been used to increase the workspace of the robot (such as in the Eclipse parallel robot [45]) and to deal with singularities [65]. The main unsolved problem for redundant parallel robot is to determine how to use the redundancy for an optimal use of the robot.

Joints

Parallel robots require higher kinematic pairs with relatively large amplitude of motion and, in some cases, relatively high load. Current available joints (either ball-and-socket or U-joints) are not completely satisfactory from this view point, although recent products like the INA joints have been developed especially for parallel robots [25]. Hence the development of higher kinematic pairs with 2 to 4 DOF is a key issue [4, 81]. As for any mechanical joints these joints must have a low friction, no hysteresis and must have a very reduced backlash. But in addition these joints must be designed so that it is possible to add sensors to measure partly or totally the amplitude of the motion of the joints, which is important for the forward kinematics.

Compliant joints are also an interesting field of research, especially for micro-robots [62].



Forward kinematics

The biggest kinematics problem is parallel robotics is the forward kinematics, which consists in finding the possible position of the platform for given joint coordinates. The forward kinematics is a more complex problem than its dual inverse kinematics counterpart for serial robots. The need of the forward kinematics is a controversial question. It may be thought that forward kinematics is an academic question that may be useful only for off-line simulation purposes and a parallel robot will be position controlled using inverse kinematics only. Pure position control is very difficult for parallel robots, especially when there are constraints on both the trajectory and the velocity of the robot (for example when the robot is used as a machine tool). In that case velocity control, which implies solving the forward kinematics, will be much more appropriate.

Although there is much mechanical architecture of parallel robots the forward kinematics problem for most of them may be reduced to solve the forward kinematics problem for a few key architectures. For example solving the forward kinematics for the Gough platform [64] allows to solve the forward kinematics of the Hexa [68] or the Hexaglide [37, 17, 36] although the mechanical architectures of these robots are quite different.

It is now well known that the forward kinematics of the Stewart-Gough platform may have up to 40 solutions and that all these 40 solutions may be real. Numerous works have provided a deep understanding of the problem which in turn has led to efficient algorithms for determining all the solutions of the forward kinematics using elimination, Gröebner basis or interval analysis. Although impressive progress has been made these algorithms are not yet real-time and furthermore it cannot be said that forward kinematics is a fully solved problem. The research continues with the works [58, 100, 40, 30, 79], etc.

The true forward kinematics problem is to determine the current position of the platform being given the joint coordinates. The algorithms provide all the solutions and hence it is necessary to sort the solutions to determine the current position. In fact the true unsolved forward kinematics problem is combination of the current algorithms with a sorting algorithm that will reject solutions that cannot be realized physically because of the presence of singularity or of the possible interferences on the trajectory. Also it is unclear if this will be sufficient to eliminate all solutions, or only one.

Another approach to solve the forward kinematics is to add extra sensors to the robot. Each extra sensor will provide an additional equation, leading to an over-constrained system which hopefully will have a unique solution. The problem is here to determine the minimal number of sensors and their location in order to have a unique solution with the simplest analytic form and quite robust with respect to the sensor errors. Some of these problems have been analyzed in [8, 45, 29] but this issue is far from being solved.

Adding extra sensors may play also an important role in the robot calibration.

Singularity analysis

There are various ways to introduce the concept of singularities but the most spectacular one is to consider the static behaviour of the robot. Let F be the wrench applied on the platform of the robot and τ the set of joint forces. These quantities are linearly related by

$$F = J^{-T}(X)\tau \quad (1)$$

where J^{-T} is the transpose of the inverse Jacobian matrix of the robot that is position dependent. Each component of the joint forces vector τ_i may be obtained as a ratio:

$$\tau_i = \frac{A}{|J^{-T}|} \quad (2)$$

where A is the minor associated to τ_i . Hence, if A is not 0, the joint force τ_i will go to infinity at any position, called singular position, where the determinant of J^{-T} is 0, causing a breakdown of the robot (in fact the breakdown will occur before reaching the singularity).

Although the condition $|J^{-T}|$ seems to be a simple condition as the matrix J^{-T} has an analytical form, the full calculation of this determinant leads to a complex expression with a large number of terms (especially if the robot has 6 DOF).

This remains an important topic of study although many progress have been made in this field, for example the geometrical classification of the singularities or algorithms for detecting singularities in a given workspace [59]. We should also mention the works of other authors dealing with singularities for different types of parallel robot manipulators like [44, 13, 2, 3, 83, 95, 96, 47, 102, 103, 51, 41].

Singularities for different configurations of parallel robots still remains open field for research.

Another open question is global analysis of singularity in relation with the workspace and trajectory planning. In that field we should mentioned the work of [24].

Workspace

One of the main drawbacks of parallel robots are their reduced workspace. Furthermore computing this workspace is not an easy task. Opposite of classical serial robots, here the translational and orientation workspace are coupled. Classically a first approach to solve this problem is to fix the values of some DOF until only 3 DOF are free. This is usually done by fixing either the orientation of the platform or the location of its centre. In the first case the geometrical approach that determine geometrically the possible motion of the centre of the platform for each kinematic chains leads usually to the best result as it provides exact calculation with a compact storage and easy representation.

Orientation workspace is more difficult to deal with as there is no universal way to represent this workspace. Here we could mention the works [7] and [70].

Another approach is to calculate an approximation either of the border or of the whole workspace using a numerical method. Some of these approaches have the advantage to be able to deal also with limits on the motion of the passive joints and to allow for workspace verification (i.e. to check if a desired workspace is included in the workspace of the robot). They may also calculate various types of workspace.

Analysis of the workspace for different types of parallel robots is given in [20, 6, 54, 96, 24, 49, 71, 72].

Workspace analysis for different configurations of parallel robots still remains open research field.

Other unsolved problems are:

- ❖ a fast algorithm to compute the maximal motion of the platform
- ❖ an algorithm that allows to check for links interference. This is a much more complex problem than may be thought in the first moment. It is necessary to determine all the hyper-surfaces in the workspace for which a pair of kinematic chain intersects in order to split the workspace in interference-free regions and then to determine in which region the initial assembly modes is located to obtain the interference-free workspace of the robot. This is a difficult task even for robot with very simple kinematic chains [15].

Motion (trajectory) planning

Motion planning is a classical problem for serial robots. But in the case of parallel robots the problem is somewhat different. For serial robot obstacle avoidance is the main reason for motion planning, but for parallel robot is the workspace. Possible problems are:

- ❖ verification if a given trajectory lie completely within the workspace of the robot
- ❖ determine if two positions may be reached by a singularity free and interference free trajectory that lie completely within the workspace of the robot

Problem 1 can be solved for almost any arbitrary time-function trajectory using interval analysis [59], while problem 2 has some particular solutions [22, 24, 82, 85]. A lot of work has to be done in this area.

Calibration

Although this problem has been solved for serial robots, this is not the case for parallel robots. Indeed, for a serial robot, small errors in the geometric parameters of the robot lead, in general, to a large difference between the real position of the end-effector and the expected one. This difference may be evaluated by measuring the position of the end-effector and then be used in an optimization procedure which will determine values of the parameters decreasing the positioning errors. Applied to parallel robot this method leads to calibration result that are in general disastrous. One of the

advantages of parallel robot is that large errors in geometric parameters may lead to quite small errors in the position of the end-effector. Furthermore the measurement noise has a large influence on the results of the calibration process.

There are two types of calibration methods:

- ❖ **external:** an external measurement device is used to determine (completely or partially) what is the real position of the platform for different desired configurations of the platform. The differences between the measured position and the desired position give an error signal that is used for the calibration [92, 105, 27, 86, 73, 74, 75, 76, 42, 23, 80, 87].
- ❖ **self-calibration:** the platform has extra sensors (for example sensors that are used for the FK) and only the robot measurements are used for the calibration [63, 101, 27, 38].

The first method is difficult and tedious to use in practice but usually gives good results. The second method is less accurate, but is easy to use and has also the advantages that it can be fully automated.

An interesting theoretical problem is to determine what are the measurement configurations of the platform that will lead to the best calibration. Of course there is an open problem to put the calibration in use in a real, industrial environment.

Dynamics

Another advantage of parallel robots is that they can reach a high acceleration and velocity, due to low mass of the moving elements [37, 17].

A first problem here is to determine appropriate dynamic model of the robot. Various formulations may be used [56, 43, 97, 61, 48, 28], although some simplifying assumption have to be made.

A second problem is implementation of control algorithms, so that the use of the parallel robot dynamic model, will really improve the motion control of the robot, compared to more classical control laws [17, 37, 36, 32, 91, 14, 39, 78, 46, 88, 5, 77].

Computing the dynamic model of a parallel robot is time consuming (and involves also solving the forward kinematic problem). An important problem here is to determine what should be the computation time of the calculation of the dynamic model, so that its use in a control loop will really leads to an improvement of the performances of the robot. This is a very complex issue especially if it is considered that the control algorithm is not continuous.

Synthesis and optimal design

It is well known that the performances that will be reached by any mechanism depends upon:

- ❖ the **topology** of the mechanism
- ❖ the **dimensions** of the components of the mechanism

This is especially true for closed-loop, parallel, mechanisms that are **highly sensitive** to both factors. When we design a parallel mechanism so that its performances should best fit to the list of requirements, both aspects must be take into consideration:



❖ *topological synthesis* i.e. finding the general arrangements of joints, links that will describe the general kinematics of the structure.

❖ *dimensional synthesis* i.e. finding the appropriate dimensioning of the mechanism.

Synthesis of parallel robot is an open field (there are very limited number of papers dealing with this problem) [1, 9, 26, 57] and the main task for the development of parallel robots in practice.

The problems caused by using parallel structures in the field of machine-tool has shown that designers which have a deep understanding of open-loop mechanisms but, have not experience in closed-loop are focused only on the development of the basic mechanical components of their machine and have almost completely neglected the analysis part.

Topology synthesis is a very complex problem for parallel mechanisms at the opposite of open-loop mechanisms for which the number of possible kinematic combinations is relatively reduced. Currently topological synthesis for parallel robots is restricted to find a mechanism with a given number of DOF without considering other performance criterion(s)

Parallel mechanisms, robots, are highly sensitive to dimensioning. One classical example given by [59] is that by changing the radius of the platform of Stewart-Gough platform by 10% we may change the minimal stiffness of the robot over its workspace by 700% .

According, [59] none of existing dimensional synthesis methods are appropriate for parallel robots which have usually a large number of design parameters. Furthermore these methods lead to a unique solution: in the case of parallel robots usually will not be a single solution to a design problem and providing only one design solution is not realistic. The main difficulty comes from the criterions which have to be considered: some of them are antagonistic (workspace and accuracy-a very accurate robot will usually have a small workspace and vice-versa), or not continuous (no singularity within the workspace), etc.

Therefore a design methodology should provide not only one single solution but, if possible, all the possible design solutions, or, at least, an approximation of the set of all design solutions.

With the optimal design (also includes topological synthesis and dimensional synthesis) which is crucial issue for development efficient parallel robots, several interesting problems could be solved, like optimization of:

- ❖ *robot kinematics* (workspace, accuracy, maximal motion of the passive joints, dexterity, accessibility, motion pattern, kinematic error)
- ❖ *robot dynamic* (robot max acceleration, robot max speed, inertia, centre of mass)
- ❖ *robot flexibility* (robot stiffness and robot natural frequencies).

Optimal design is open and actual problem. Very few papers could be find in this area [66, 67, 52, 53, 12, 34].

Controller

Parallel robot will be effective system only if the robot controller allows dealing with the specific characteristics of parallel robots. Unfortunately the current trend, especially in the field of machine tools, is adaptation of existing hardware for the purpose of controlling parallel robots.

If may be, this trend could be justified at the beginning of parallel robotics, long term this will have very bad effect on the robot performances.

Analysis in the machine-tool field have shown that more of the 70% errors on the fabricated parts are induced by controller, CAD system is responsible of approximately 20% of the errors, and the Stewart-Gough platform (if optimally designed) less than 10% [59]. Hence research should be focused mostly on the controller. The hardware of the controller should support:

- ❖ the possibility of using appropriate control laws capable to deal with inherent non-linearities of parallel robots,
- ❖ parallel computation (that will drastically improve the sampling time)
- ❖ specialized integrated circuits that will be devoted to basic computation tasks such as inverse and forward kinematics

CONCLUSION

In this paper we notified some open questions in parallel robotics. Some of the problems are long term, but others should be solved as soon as possible in order to enable wider application of parallel robots in practice.

Serial and parallel robots probably will live parallel a long years. If we compare about 20 years research in parallel mechanisms and more than 200 years in research to reach the current level of knowledge for serial mechanisms, it is easy to conclude that this process of solving problems in parallel robotics will be long term.

ACKNOWLEDGMENT

This research was done at the Department of Machine Tools and Automation, TU Hamburg-Harburg, Germany, financed by DFG (Deutsche Forschungs-gemeinschaft).

REFERENCES

- [1] ANGELES J., 2002. *The Qualitative Synthesis of Parallel Manipulators*, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators October 3–4, 2002, Quebec City, Quebec, Canada pp.160-168
- [2] ANGELES J., YANG G., CHEN I. M., 2001. *Singularity Analysis of Three-Legged, Six-DOF Platform Manipulators with RRRS Legs*, 2001 IEEE/ASME International Conference on Advanced Intelligent Mechatronics Proceedings, 8-12 July 2001, Como, Italy, pp.32-36
- [3] ANGELES J., YANG G., CHEN I. M., 2003. *Singularity Analysis of Three-Legged, Six-DOF Platform Manipulators With URS Legs*, IEEE/ASME TRANSACTIONS ON MECHATRONICS, VOL. 8, NO. 4, DECEMBER 2003, pp.469-475
- [4] ANNACONDA, E., APILE, E., DOTTA, A., BOËR, C. R., 2002. *An Experience in Design and Development of Joints for Parallel Kinematics Machines*, The 3rd Chemnitz Parallel Kinematics Seminar PKS 2002, Chemnitz, Germany, pp.243-261

- [5] BELDA K., 2004, *Various utilization of predictive control, in parallel machine tools*, 5th International PhD Workshop on Systems and Control a Young Generation Viewpoint September 8-11, 2004 Balatonfüred, Hungary
- [6] BONEV A. I., RYU J., 1999, *Workspace Analysis Of 6-Prts Parallel Manipulators Based On The Vertex Space Concept*, Proceedings of the 1999 ASME Design Engineering Technical Conferences September 12-15, 1999, Las Vegas, Nevada, DETC99/DAC-8647
- [7] BONEV A. I., RYU J., 2003, *A new approach to orientation workspace analysis of 6-DOF parallel manipulators*, Mechanism and Machine Theory 36 (2001) pp.15-28
- [8] BONEV A. I., RYU J., KIM S. G. AND LEE S. K., 2001, *A Closed-Form Solution to the Direct Kinematics of Nearly General Parallel Manipulators with Optimally Located Three Linear Extra Sensors*, TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 17, NO. 2, APRIL 2001, pp.148-156
- [9] BROGARDH T., 2002, *PKM Research - Important Issues, as seen from a Product Development Perspective at ABB Robotics*, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators October 3-4, 2002, Quebec City, Quebec, Canada, pp.68-82
- [10] BRUZZONE L., MOLFINO R.M., AND ZOPPI M., 2004, *Kinematic modelling and simulation of a novel interconnected-chains PKM*, Int. Conf. Modelling, Identification and Control MIC2004, Grindelwald, Switzerland, February 23-25 2004. ISBN 0-88986-387-3.
- [11] CASTELLI P. V. AND DI GREGORIO R., 2000, *Influence of manufacturing errors on the kinematic performance of the 3-UPU parallel mechanism*, 2nd Chemnitz Parallelkinematik Seminar, pages 85-99, Chemnitz, Germany, 2000.
- [12] CECCARELLI M., CARBONE G. AND OTTAVIANO E., 2005, *Multi criteria optimum design of manipulators*, BULLETIN of the POLISH ACADEMY of SCIENCES, TECHNICAL SCIENCES, Volume 53, Issue 1, March 2005, pp 9 - 18
- [13] CHEN S.-L. AND YOU I.-T., 2000, *Kinematic and Singularity Analyses of a Six DOF 6-3-3 Parallel Link Machine Tool*, Int J Adv Manuf Technol (2000) 16:835–842
- [14] CHUANG H. Y. AND CHANG Y. C., 2001, *Evaluation of an Adaptive Weighting Cross-Coupled Controller for a 3-PRPS Platform*, ISME International Journal Series C, Vol. 44 (2001), No. 1, pp. 164-170
- [15] CHUCKPAIWONG I., NEWMAN S. W., 2001, *Reflexive collision avoidance for a Novell parallel Mnaipulator*, Proceedings of the 2001 IEEE/RSJ, International Conference on Intelligent Robots and systems, Maui, Hawaii, USA, Oct. 29-Nov.03, 2001, pp.1293-1298.
- [16] CLAVEL R., THURNEYSSEN M., GIOVANOLA J., SCHNYDER M., JEANNERAT D., 2002, *HITA-STT A new 5 dof parallel kinematics for production applications*, Proceedings of the 33rd ISR (International Symposium on Robotics) October 7 – 11, 2002
- [17] CODOUREY A., HONEGGER M., BURDET E., 1997, *A Body-oriented Method for Dynamic Modeling and Adaptive Control of Fully Parallel Robots*, SYROCO'97, Nantes, France, September 1997
- [18] COMPANY O., KRUT S. AND PIERROT F., 2002, *Modeling and Preliminary Design Issues of a 4-Axis Parallel Machine for Heavy Parts Handling*, IMechE Journal of Multibody Dynamics, Vol. 216, Special Issue, Part K, pp. 1-11, January 2002.
- [19] COMPANY O., PIERROT F., 1999, *A new 3R-1T parallel robot*, 9th International Conference on Advanced Robotics, Tokyo, Japan, 25-27 October 1999, pp. 557-562.
- [20] CONTI J.P., CLINTON C.M., ZHANG G., WAWERING A.J., 1998, *Workspace Variation of a Hexapod Machine Tool*, Published: NISTIR 6135, National Institute of Standards and Technology, Gaithersburg, MD, March 1998
- [21] CORRADINI C., FAUROUX J.-C., KRUT S. AND COMPANY O., 2003, *Evaluation of a 4-Degree of Freedom Parallel Manipulator Stiffness*, 11th World Congress in Mechanism and Machine Science, Tianjin, China, August 2003.
- [22] CORTÉS J. AND SIMÉON T., 2003, *Probabilistic Motion Planning for Parallel Mechanisms*, Proc. of the IEEE International Conference on Robotics and Automation, 2003.
- [23] DANEV D., PAPEGAY Y., NEUMAIER A., 2004, *Interval Methods for Certification of the Kinematic Calibration of Parallel Robots*, Proceedings of the 2004 IEEE International Conference on Robotics & Automation, New Orleans, LA • April 2004 pp.1913-1918
- [24] DASH, A.K., CHEN, I.-M., YEO, S.H., YANG, G.L., 2002, *Workspace Analysis and Singularity-free Path Planning of Parallel Manipulators*, Int'l Conf. Mechatronics Technology, Fukuoka, Japan, pp. 457-462, 2002.
- [25] DÜRSCHMIED, F., HESTERMANN, J.-O., 2002, *Achieving Technical and Economic Potential with INA Components*, The 3rd Chemnitz Parallel Kinematics Seminar PKS 2002, Chemnitz, Germany, pp.263-275
- [26] FANG Y., TSAI L.-W., 2002, *Structure Synthesis of a Class of 4-DoF and 5-DoF Parallel Manipulators with Identical Limb Structures*, THE INTERNATIONAL JOURNAL OF ROBOTICS RESEARCH, September 2002, pp. 799-810
- [27] FASSI I., LEGNANI G., 2002, *Automatic Identification of a Minimum, Complete and Parametrically Continuous Model for the Geometrical Calibration of Parallel Robots*, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators October 3-4, 2002, Quebec City, Quebec, Canada, pp.204-214
- [28] GALLARDO J., RICO J.M., FRISOLI A., CHECCACCI D., BERGAMASCO M., 2003, *Dynamics of parallel manipulators by means of screw theory*, Mechanism and Machine Theory 38 (2003) pp. 1113–1131
- [29] GAO J., WEBB, P AND GINDY N., 2003, *Error reduction for an inertial-sensor-based dynamic parallel kinematic machine positioning system*, INSTITUTE OF PHYSICS PUBLISHING MEASUREMENT SCIENCE AND TECHNOLOGY, Meas. Sci. Technol. 14 (2003) pp.543–550
- [30] GAO X.-S., LEI D., LIAO Q., ZHANG G.-F., 2005, *Generalized Stewart–Gough Platforms and Their Direct Kinematics*, IEEE TRANSACTIONS ON ROBOTICS, VOL. 21, NO. 2 APRIL 2005, pp.141-150
- [31] GOUGH V. E., WITEHALL S. G., 1962, *Universal Tire Test Machine*, Proceedings of the 9th International Automobile Technical Congress FISITA, London (UK), ImechE (pp. 117 – 137) 1962.
- [32] GRAF R., VIERLING R., DILLMANN R., 1998, *A flexible controller for a Stewart platform*, 2nd Int. Conf. on knowledge-based intelligent electronic Systems, Adelaide, 21-23 April 1998, pp. 52-59
- [33] GREGÓRIO D. R., CASTELLI P. V., 2002, *Geometric Error Effects on the Performances of a Parallel Wrist*, The 3rd Chemnitz Parallel Kinematics Seminar PKS 2002, pp. 1011-1024
- [34] HAO F., MERLET J.-P., 2005, *Multi-criteria optimal design of parallel manipulators based on interval analysis*, Mechanism and Machine Theory 40 (2005) 157–171
- [35] HAYES M. J. D., MURRAY P. J. Z., CHEN C., 2004, *Unified Kinematic Analysis of General Planar Parallel Manipulators*, Journal of Mechanical Design 2004 by ASME, September 2004, Vol. 126, pp.1-10
- [36] HONEGGER M., 1998, *Nonlinear adaptive control of a 6-DOF parallel manipulator*, MOVIC '98, Zurich, Switzerland, August 25-28, vol. 3, pp. 961-966, 1998
- [37] HONEGGER M., CODOUREY A., BURDET E., 1997, *Adaptive Control of the Hexaglide, a 6 dof Parallel Manipulator*, IEEE International Conference on Robotics and Automation, Albuquerque, USA, April 1997
- [38] HSU W.-Y., CHEN J.-S., 2004, *Error analysis and auto-calibration for a Cartesian-guided tripod machine tool*, Int J Adv Manuf Technol (2004) 24: pp. 899–909
- [39] HUBERT H., 2003, *Model Based Control of a Parallel Robot – A Comparison of Control Algorithms*, PAMM · Proc. Appl. Math. Mech. 2, (2003), pp.124–127
- [40] JAKOBOVIC D., BUDIN L., 2002, *Forward Kinematics of a Stewart Platform Mechanism*, INES 2002, 6th International Conference on Intelligent Engineering Systems 2002, Opatija, Croatia
- [41] JIN Y., CHEN I.-M., YANG G., 2004, *Structure synthesis and singularity analysis of a parallel manipulator based on selective actuation*, Proceedings of IEEE Int. Conf. on



- Robotics and Automation, pages 4533-4538, New Orleans, 28-30 April 2004
- [42] JOSHI, S., SURIANARAYAN, A., 2003, Calibration of a 6-DOF Cable Robot Using Two Inclinometers, Performance Metrics for Intelligent Systems, PerMIS '03, NIST Special Publication 1014, September 16 - 18, 2003
- [43] KHALIL W., GUEGAN S., 2001, A New Method for the Dynamic Formulation of Parallel Manipulators, Journées Franco-Mexicaines d'automatique appliquée, 12-14 Septembre, 2001
- [44] KIM D. AND CHUNG, W., 1999, Analytic Singularity Equation and Analysis of Six-DOF Parallel Manipulators Using Local Structurization Method, IEEE TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 15, NO. 4, AUGUST 1999, pp.612-622
- [45] KIM J., PARK F. C., RYU S. J., KIM J., HWANG J. C., PARK C., AND IURASCU C. C., 2001, Design and Analysis of a Redundantly Actuated Parallel Mechanism for Rapid Machining, IEEE TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 17, NO. 4, AUGUST 2001, pp.423-434
- [46] KOHN N., KOLBUS M., REISINGER T., DIETHERS K., STEINER J., THOMAS U., 2004, PROSA - A Generic Control Architecture for Parallel Robots, Proceedings of the Mechatronics & Robotics, Aachen, September 2004
- [47] KONG X., GOSSELIN C. M., 2002, Kinematics and Singularity Analysis of a Novel Type of 3-CRR 3-DOF Translational Parallel Manipulator, The International Journal of Robotics Research, Vol. 21, No. 9, September 2002, pp. 791-798,
- [48] KOVEČSES J., PIEDBOEUF J.-C., LANGE C., 2002, Methods for Dynamic Models of Parallel Robots and Mechanisms, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators October 3-4, 2002, Quebec City, Quebec, Canada, pp.339-347
- [49] LIN C., TANG X., SHI J., DUAN G., 2003, Workspace analysis of reconfigurable parallel machine tool based on setting-angle of spherical joint Systems, Man and Cybernetics, 2003, IEEE International Conference on Volume 5, 5-8 Oct. 2003 Page(s): pp. 4945 - 4950 vol.5
- [50] LIU X.-J., KIM J., WANG J., 2002, Two Novel Parallel Mechanisms with Less than Six DoFs and the Applications, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators, October 3-4, 2002, Quebec City, Quebec, Canada, pp.172-178
- [51] LIU G., LOU Y., AND LI, Z. 2003, Singularities of Parallel Manipulators: A Geometric Treatment, IEEE TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 19, NO. 4, AUGUST 2003 pp.579-594
- [52] LOU Y. ET AL., 2004, A general approach for optimal kinematic design of parallel manipulators, Proceedings of the IEEE Int. Conf. on Robotics and Automation, pp. 3659-3664, New Orleans, 28-30 April 2004
- [53] LOU Y.J., LIU G.F., AND LI Z.X., 2005, A General Approach for Optimal Design of Parallel Manipulators, SUBMIT TO IEEE TRANSACTIONS ON AUTOMATION SCIENCE AND ENGINEERING, VOL. X, NO. X, XX 2005
- [54] MAJID M. Z. A., HUANG Z. AND YAO Y. L., 2000, Workspace Analysis of a Six-Degrees of Freedom, Three-Prismatic-Prismatic-Spheric-Revolute Parallel Manipulator, Int J Adv Manuf Technol (2000) 16: pp. 441-449
- [55] MARQUET F., COMPANY O., KRUT S. AND PIERROT F., 2002, Enhancing Parallel Robots Accuracy with Redundant Sensors, IEEE ICRA: Int. Conf. on Robotics and Automation, Washington, DC, USA, Mai 11-15, 2002, pp. 4114-4119
- [56] MCAREE P. R., SELIG J. M., 1999, Constrained Robot Dynamics II: Parallel Machines, Journal of Robotic Systems 16(9), 487-498 (1999)
- [57] MENG J., LIU G., LI Z., 2005, A Geometric Theory for Synthesis and Analysis of Sub-6 DoF Parallel Manipulators, International Conference on Robotics and Automation, April 18-2005, Barcelona, Spain
- [58] MERLET J.-P., 1999, Forward kinematics of parallel robots, Proceedings of IMACS Conf. on Applications of Computer Algebra, El Escorial, 24-27 June 1999
- [59] MERLET J. P., 2000, Parallel robots, Kluwer, 2000
- [60] MERLET J.-P., 2002, An initiative for the kinematics study of parallel manipulators, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators, October 3-4, 2002, Quebec City, Quebec, Canada, pp.1-9
- [61] MILLER K., 2001, Dynamics of the New UWA Robot, ACRA 2001, Australian Conference on Robotics and Automation, Sydney, 14 - 15 November 2001, pp.1-6
- [62] MOON Y.-M., KOTA S., 2002, Design Of Compliant Parallel Kinematic Machines, Proceedings of DETC 02, ASME 2002 Design Engineering Technical Conferences and Computer and Information in Engineering Conference Montreal, Canada, September 29-October 2, 2002
- [63] NAHVI A., HOLLERBACH J.M., HAYWARD V., 1994, Calibration of a parallel robot using multiple kinematics closed loops, Proceedings of the IEEE Int. Conf. on Robotics and Automation, San Diego, 8-13 May 1994, pp. 407-412,
- [64] NANUA P., WALDRON K.J., 1989, Direct kinematic solution of a Stewart platform, Proceedings of the IEEE Int. Conf. on Robotics and Automation, Scottsdale, 14-19 May 1989, pp. 451-457
- [65] O'BRIEN J., WEN J. T., 1999, Redundant Actuation for Improving Kinematic Manipulability, 1999 IEEE International Conference on Robotics and Automation, May 10-15, 1999, Marriott Hotel, Renaissance Center, Detroit, Michigan, Proceedings, IEEE Robotics and Automation Society 1999, Volume, 2 pp. 1520-1525
- [66] OTTAVIANO E. AND CECCARELLI M., 2001, Optimal Design of CaPaMan (Cassino Parallel Manipulator) With Prescribed Position and Orientation Workspace, Proceedings of the IEEE 9th Mediterranean Conference on Control and Automation, June 27-29, 2001, Dubrovnik, Croatia
- [67] OTTAVIANO E. AND CECCARELLI M., 2002, Optimum Design of Parallel Manipulators for Workspace and Singularity Performances, Proceedings of the WORKSHOP on Fundamental Issues and Future Research Directions for Parallel Mechanisms and Manipulators, 2002, Quebec City, Quebec, Canada, pp.98-105
- [68] PIERROT F., DAUCHEZ P., AND FOURNIER A., 1991, Hexa: a fast six-dof fully parallel robot, Proceedings of ICAR conference, 1991, pp. 1159-1163.
- [69] PIERROT F., MARQUET F., COMPANY O., GIL T., 2001, H4 parallel robot: modelling, design and preliminary experiments, IEEE Int. Conf. On Robotics and Automation, Seoul, Korea, May 2001
- [70] POTT A., FRANITZA D., HILLER M., 2004, Orientation workspace verification for parallel kinematic machines with constant leg length, Proceedings of Conference Mechatronics and Robotics, MechRob 2004, Aachen, 2004
- [71] PUSEY J., FATTAH A., AGRAWAL S., MESSINA E. AND JACOFF A., 2003, Design and Workspace Analysis of a 6-6 Cable-Suspended Parallel Robot, Proceedings of the 2003 IEEE/RSJ Intl. Conference on Intelligent Robots and Systems Las Vegas, Nevada · October 2003, pp.2090-2095
- [72] PUSEY J., FATTAH A., AGRAWAL S., MESSINA E., 2004, Design and workspace analysis of a 6-6 cable-suspended parallel robot, Mechanism and Machine Theory 39 (2004) 761-778
- [73] RENAUD P., ANDREFF N., GOGU G., 2003-1, On Vision-based Kinematic Calibration of a Stewart-Gough Platform, Proceedings of the 11th World Congress in Mechanism and Machine Science, August 18.21, 2003, Tianjin, China
- [74] RENAUD P., ANDREFF N., GOGU G., DHOME M., 2003-2, Optimal pose selection for vision-based kinematic calibration of parallel mechanisms, IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS'2003), pp. 2223-2228, vol. 3, Las Vegas, USA, October 2003,
- [75] RENAUD P., ANDREFF N., MARQUET F., MARTINET P., 2003-3, Vision-based Kinematic Calibration of a H4 parallel mechanism, 2003 IEEE International Conference on Robotics and Automation, pp. 1191-1196, Taipei, Taiwan, September 2003,



- [76] RENAUD P., ANDREFF N., KRUT S., GOGU G., 2004, Kinematic calibration of linear-actuated parallel mechanisms from leg observation, 35th International Symposium on Robotics, April 2004, Paris, France.
- [77] RIDGEWAY, S., AND CRANE, C., 2004, Control Considerations in the Design of a Parallel Kinematic Machine with Separate Actuation and Metrology Mechanisms, Proceedings of the 12th Mediterranean Conference on Control and Automation (MED '04), Kusadasi, Turkey, June 2004.
- [78] SABATER, J.M., AZORIN, J.M., GARCIA, N., ARACIL, R., SALTAREN, R., 2003, Kinematics control of a 6 URS parallel platform working as an impedance display, 2003 IEEE Conference on Control Applications
- [79] SADJADIAN H., TAGHIRAD H.D., FATEHI A., 2005, Neural Networks Approaches for Computing the Forward Kinematics of a Redundant Parallel Manipulator, International Journal of Computational Intelligence Volume 2 Number 1 2005, PP.40-47
- [80] SATO O., SHIMOJIMA K., OLEA G., FURUTANI R., TAKAMASU K., 2004, Full Parameter Calibration of Parallel Mechanism, 4th International Conference of the European Society for Precision Engineering and Nanotechnology (euspen2004, Glasgow, UK, May 31 - June 2), 2004, 396-39
- [81] SCHNYDER, M.; GIOVANOLA, J.; CLAVEL, R.; THURNEYSEN, M.; JEANNERAT, D., 2004, Spherical Joints with 3 and 4 Degrees of Freedom for 5-Axis Parallel Kinematics Machine Tool, The 4 Chemnitz Parallel Kinematics Seminar PKS2004, Chemnitz, Germany, April 20-21, 2004, pp.487-502
- [82] SHAW D. AND CHEN Y.-S., 2001, Cutting path generation of the Stewart-Platform-Based Milling Machine using an end-mill, Int. J. Prod. Res., 2001, vol. 39, no. 7, pp.1367-1385
- [83] SIMAAN N. AND SHOHAM M., 2001, Singularity Analysis of a Class of Composite Serial In-Parallel Robots, IEEE TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 17, NO. 3, JUNE 2001 pp. 301-311
- [84] STEWART, D., 1965, A Platform with Six Degrees of Freedom, Proc. Inst. Mech. Eng. London, Vol 180, 1965, pp. 371-386.
- [85] SU H., DIETMAIER P., MCCARTHY J. M., 2003, Trajectory Planning for Constrained Parallel Manipulators, ASME Journal of Mechanical Design, March 2003
- [86] TAKAMASU K., MURUI I., SATO O., OLEA G. AND FURUTANI R., 2002, Calibration of Three Dimensional Mechanism - Novel Calibration Method for 3DOF Parallel Mechanism, Proceedings of IEEE ICIT'02 (Bangkok, December), 2002, pp. 394-398
- [87] TANG X., WANG J., GAO M., 2004, Kinematic calibration of gantry hybrid machine tool based on estimation error and local measurement information, Int J Adv Manuf Technol (2004) Published online: 24 November 2004
- [88] TING Y., CHEN Y.-S., AND JAR H.-C., 2004, Modeling and Control for a Gough–Stewart Platform CNC Machine, Journal of Robotic Systems 21(11), (2004), pp. 609–623
- [89] TLUSTY J., ZIEGERT J., RIDGEWAY S., 1999, Fundamental comparison of the use of serial and parallel kinematics for machine tools authors, Annals of CIRP, 48/1/1999, pp. 351-356
- [90] TSAI L. W., 1999, Robot Analysis: The Mechanics of Serial and Parallel Manipulators, New York: John Wiley & Sons, Inc., 1999.
- [91] WALKER I.D., AND BENNETT J.K., 1998, Parallel robot control using speculative computation. Journal of Robotics and Automation, 13(4), 101-112, Dec, 1998. DL Hamilton,
- [92] WU J., ZHANG L., LI S., 2001, Posture Measurement And Structural Parameters Calibration On Parallel 6 Dof Platform, Fifth International Conference On Fluid Power Transmission And Control (ICFP2001) 3-5 April, 2001, Hangzhou, China
- [93] www.delphion.com
- [94] www.fanucrobotics.com
- [95] YANG G., CHEN I.-M., LIN W. AND ANGELES J., 2001, Singularity Analysis of Three-Legged Parallel Robots Based on Passive-Joint Velocities, IEEE TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 17, NO. 4, AUGUST 2001, pp. 413-422
- [96] YIU Y.K., AND LI Z.X., 2001-1, Modeling Configuration Space and Singularities of Parallel Mechanisms, International Conference on Mechatronics Technology, 6 - 8 June 2001, Singapore pp. 298-303
- [97] YIU Y.K., AND LI Z.X., 2001-2, Dynamics of a Planar 2-dof Redundant Parallel Robot, International Conference on Mechatronics Technology, 6 - 8 June 2001, Singapore, pp.359-344
- [98] ZHANG D. AND LANG, S. Y. T., 2003, On Conceptual Design of 5-axis Parallel Kinematic Machines using kinetostatic modelling approach, 2nd International Conference on Reconfigurable Manufacturing d International Conference on Reconfigurable Manufacturing 2003
- [99] ZHAO T. S., DAI J. S. AND HUANG Z., 2002, Geometric Analysis of Overconstrained Parallel Manipulators with Three and Four Degrees of Freedom, JSME International Journal Series C, Vol. 45 (2002), No. 3, pp.730-740
- [100] ZHAO X., PENG S., 2000, Direct Displacement Analysis of Parallel Manipulators, Journal of Robotic Systems 17(6), (2000), pp.341-345
- [101] ZHUANG H., 1997, Self-Calibration of Parallel Mechanisms with a Case Study on Stewart Platforms, IEEE TRANSACTIONS ON ROBOTICS AND AUTOMATION, VOL. 13, NO. 3, JUNE 1997, pp.387-397
- [102] ZLATANOV, D., BONEY, I.A., GOSSELIN, C.M., 2002, Constraint Singularities as C-Space Singularities, 8th International Symposium on Advances in Robot Kinematics (ARK 2002), Caldes de Malavella, Spain, 24–28 June, 2002.
- [103] ZOPPI M., BUZZONE L. E., MOLFINO R. M., NICHELINI R. C., 2003, Constraint Singularities of Force Transmission in Nonredundant Parallel Robots With Less Than Six Degrees of Freedom, Journal of Mechanical Design 2003 SEPTEMBER 2003, Vol. 125, pp. 557-563
- [104] ZOPPI M., BRUZZONE L., MOLFINO R.M., 2004, A novel 5-DoF Interconnected-Chains PKM for manufacturing of revolute surfaces, The 4 Chemnitz Parallel Kinematics Seminar PKS2004, April 20-21, 2004, Chemnitz, Germany, pp.437-448
- [105] ZOU H., NOTASH L., 2001, Discussions on the Camera-Aided Calibration of Parallel Manipulators, 2001 CCToMM Symposium on Mechanisms, Machines, and Mechatronics 2001 CCToMM SM, June 1, 2001, the Canadian Space Agency, Saint-Hubert (Montréal), Québec, Canada

AUTHORS & AFFILIATION

Zoran PANDILOV¹,
Vladimir DUKOVSKI²

^{1,2}UNIVERSITY "SV. KIRIL I METODIJ", FACULTY OF MECHANICAL ENGINEERING-SKOPIJE, KARPOS II B.B., P.O.BOX 464, MK-1000, SKOPIJE, REPUBLIC OF MACEDONIA

